

EEEC 603  
MICROWAVE ENGINEERING

UNIT-1

# Applications of circular waveguide

- Rotating joints in radars to connect the horn antenna feeding a parabolic reflector (which must rotate for tracking)
- $TE_{01}$  mode suitable for long distance waveguide transmission above 10 GHz.
- Short and medium distance broad band communication (could replace / share coaxial and microwave links)

# Waveguide components



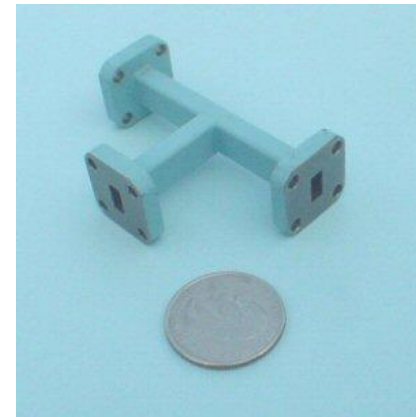
Rectangular waveguide



Waveguide to coax adapter



Waveguide bends



E-tee

# Uses

- To reduce attenuation loss
  - High frequencies
  - High power
- Can operate only above certain frequencies
  - Acts as a High-pass filter
- Normally circular or rectangular
  - We will assume lossless rectangular

# Modes of propagation

From these equations we can conclude:

- TEM ( $E_z=H_z=0$ ) can't propagate.
- TE ( $E_z=0$ ) transverse electric
  - In TE mode, the electric lines of flux are perpendicular to the axis of the waveguide
- TM ( $H_z=0$ ) transverse magnetic,  $E_z$  exists
  - In TM mode, the magnetic lines of flux are perpendicular to the axis of the waveguide.
- HE hybrid modes in which all components exists

# Dominant Mode

- The dominant mode is the mode with lowest cutoff frequency.
- It's always  $TE_{10}$
- The order of the next modes change depending on the dimensions of the guide.

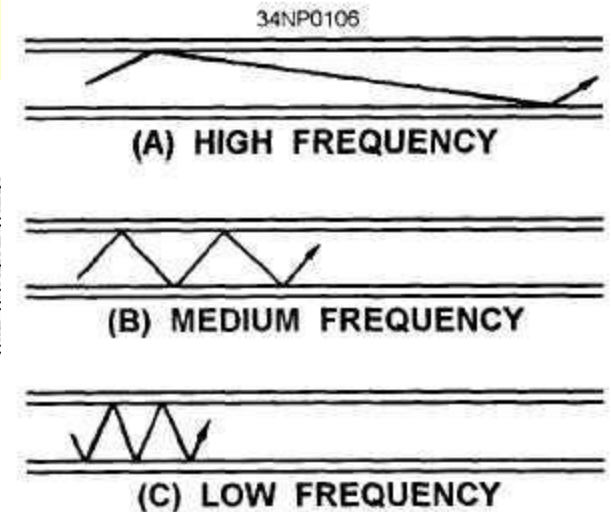
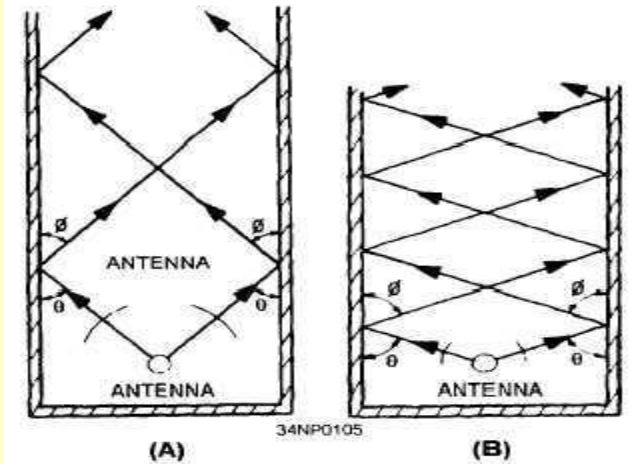
# Group velocity, $u_g$

- As frequency is increased, the group velocity increases.
- Is the velocity at which the energy travels.

$$u_g = \frac{1}{\partial\beta / \partial\omega} = u' \sqrt{1 - \left[ \frac{f_c}{f} \right]^2} \left[ \frac{\text{rad/s}}{\text{rad/m}} \right] = \left[ \frac{m}{s} \right]$$

- It is always less than  $u'$

$$u_p u_g = (u')^2$$



# Power transmission

- The average Poynting vector for the waveguide fields is

$$\begin{aligned} P_{ave} &= \frac{1}{2} \operatorname{Re}[E \times H^*] = \frac{1}{2} \operatorname{Re}[E_x H_y^* - E_y H_x^*] \\ &= \frac{|E_x|^2 + |E_y|^2}{2\eta} \hat{z} \quad [\text{W/m}^2] \end{aligned}$$

- where  $\eta = \eta_{TE}$  or  $\eta_{TM}$  depending on the mode

$$P_{ave} = \int P_{ave} \cdot dS = \int_{x=0}^a \int_{y=0}^b \frac{|E_x|^2 + |E_y|^2}{2\eta} dy dx \quad [\text{W}]$$



# Attenuation in Lossy waveguide

- When dielectric inside guide is lossy, and walls are not perfect conductors, power is lost as it travels along guide.

$$P_{ave} = P_o e^{-2\alpha z}$$

- The loss power is 
$$P_L = -\frac{dP_{ave}}{dz} = 2\alpha P_{ave}$$

- Where  $\alpha = \alpha_c + \alpha_d$  are the attenuation due to ohmic (conduction) and dielectric losses
- Usually  $\alpha_c \gg \alpha_d$

# Attenuation for $TE_{10}$

- Dielectric attenuation, Np/m

$$\alpha_d = - \frac{\sigma \eta'}{2 \sqrt{1 - \left( \frac{f_c}{f} \right)^2}}$$

Dielectric  
conductivity!

- Conductor attenuation, Np/m

$$\alpha_c = - \frac{2R_s}{b \eta' \sqrt{1 - \left( \frac{f_{c,10}}{f} \right)^2}} \left( 0.5 + \frac{b}{a} \left( \frac{f_{c,10}}{f} \right)^2 \right)$$